

Dynamical formation of resonant planetary systems with high mutual inclination

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Dedicated to the memory of J.D. Hadjidemetriou



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Overview - Motivation

- There are ~240 planetary systems with 2 or more planets (~730 planets)
- Some systems have planets in resonance (mainly 2/1, also 3/1)
- Lee & Thommes (2009) → 2/1 inclination resonance
 Libert & Tsiganis (2009): capture and inclination excitation possible in the 2/1, 3/1, 4/1 and 5/1 resonances

Q: do such '3-D' (stable) systems exist ?

• Also important to understand the distribution of non-resonant systems (resonance \rightarrow excitation \rightarrow pl-pl scattering \rightarrow "new" system forms)

Q: could we 'recognize' such systems observationally (i.e. constraints) ?

Planet migration and Resonant capture

Planets migrating at different rates \implies mean motion ratio changes if converging, resonance trapping can occur \implies planets then migrate as a pair, while keeping the MMR n_1/n_2 ~fixed.



Goal: understand what conditions need to be met for *i* to grow

Capture and evolution in resonance: 2-D case

Lee & Peale (2002): GJ876 planets in 2/1 resonance

Migration rate

Eccentricity damping

$$\frac{da_i/dt}{a_i} = -v_i, \qquad \frac{de_i/dt}{e_i} = -Kv_i$$

Ferraz-Mello, Beauge and Michtchenko (2003, 2006) \rightarrow migration forces the resonant system to follow a specific path in phase space, along stationary resonant solutions

Hadjidemetriou & Voyatzis (2010): these paths correspond to families of stable periodic orbits of the 3BP (easily computed in a rotating frame)



For given mass ratio and MMR we can predict the evolution path by computing the families of POs (and their stability character)

Q: are there critical solutions that force the system to go out of plane?



Vertical stability of POs

- Take a 2-D periodic solution $\overline{q}(t) = (x_1, x_2, y_2, 0, \dot{x_1}, \dot{x_2}, \dot{y_2}, 0)$
- Add a small vertical displacement $(|\zeta_{20}| \ll 1, |\dot{\zeta}_{20}| \ll 1)$ $q(t) = (x_{1,}x_{2,}y_{2,}\zeta_{2}, \dot{x}_{1}, \dot{x}_{2}, \dot{y}_{2}, \dot{\zeta}_{2})$
- Linearize the vertical component
 - $\ddot{z}_2 = A(\mathbf{q})z_2 + B(\mathbf{q})\dot{z}_2 \rightarrow \ddot{\zeta}_2 = A(\overline{\mathbf{q}})\zeta_2 + B(\overline{\mathbf{q}})\dot{\zeta}_2 \rightarrow \ddot{\zeta}_2 = \overline{A}(t)\zeta_2 + \overline{B}(t)\dot{\zeta}_2$
- and plug in the 2-D solution $Z = \Delta(T) Z_0$

$$(\det \Delta(T) = 1) \rightarrow \lambda^2 - (a+d)\lambda + 1 = 0, \quad k_v = \frac{1}{2}(a+d)$$

Vertical stability index

- $|k_v| < 1$: bounded solutions vertical stability
- $|k_v| > 1$: unbounded solutions vertical instability
- $|k_v|=1$: vertical critical orbits (v.c.o.)

(Henon, 1973; Michalodimitrakis, 1979)



Vertical stability and orbit evolution



Numerical experiments

• To 1st order, the effects of Type II migration can be approximated by adding a Stokes-like force to the equations of motion of the 3BP:

$$\boldsymbol{F}_{d} = -C \left(\boldsymbol{v}_{p} - a \, \boldsymbol{v}_{c} \right)$$

this gives (Beauge&Ferraz-Mello, 1993; Beauge et al 2006)



- Model : TBP + \mathbf{F}_{d}
- Starting conditions : $e_i \approx 0$, $i_i \approx 0$
- Parameters: $10^{-7} \le v \le 10^{-4} (y^{-1}), \quad 0.5 \le K \le 100$

An example







2/1 resonance : vertical critical points



2/1 resonance : different mass ratios



3/1 resonance : vertical critical points



3/1 resonance : different mass ratios



Migration parameters $v = 8 \ 10^{-7} \ y^{-1}$ $K = 1 \ (K=0.5)$

Conclusions

• *VCOs* determine the position of *inclination resonance* in the eccentricity plane

• After crossing a VCO the system follows a path that is determined by the bifurcating *3D family of periodic orbits*

evolution is 'predictable' (save for K ...)

• For 2/1 resonance captures, the inclination resonance occurs in *two* different eccentricity domains (critical mass ratio $\rho=0.43$)

- For 3/1 resonance captures V.C.Os fall *on a line* in e1-e2
- mass ratio, resonance ration and eccentricities tell us if the system has reached the critical solution (none so far...)
 a minimum effective *K* (damping) can be deduced for systems that have not passed through a VCO